

# Challenges Associated with Welding for Hydrogen Service and a Case Study

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 **CRC** EVANS

 **MICRO** ALLOYING



# Presentation Outline

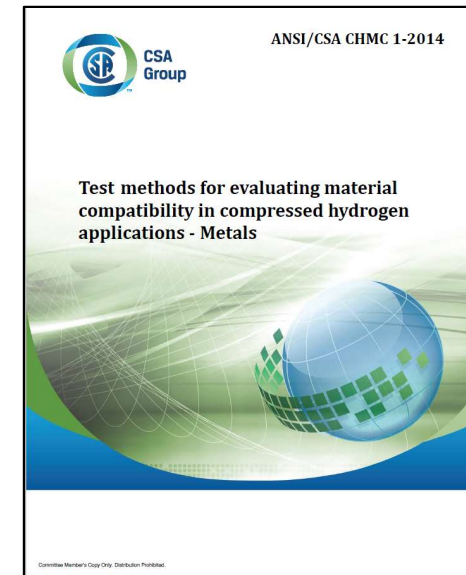
- Hydrogen Pipelines
  - Girth Weld Fracture Performance
- Hydrogen Transport Ships
  - Seam Weld Fatigue Performance

# Hydrogen Pipelines

- Major Concern with Hydrogen Pipelines is Girth Weld Performance.
  - Potential for High Local Strains / Stress
  - Presence of Girth Weld Hi-Lo Misalignment
  - Potential Presence of Girth Weld Flaws
- Unlike Liquid Pipelines, Gas Pipelines generally experience Low Fatigue Demand, particularly girth welds.
- Major concern is Fracture at Girth Welds due to High Local Stress and Reduced Toughness.
- CRC is actively engaged in the API 1104 Hydrogen Task Group to develop Girth Weld Qualification Requirements for Hydrogen Pipelines

# Hydrogen Fracture Toughness Test Methods

- 1) ASME B31.12 – 2019 “ Hydrogen Piping and Pipelines”
  - Constant Load or Constant Displacement Tests
- 2) ANSI / CSA CHMC 1-2014, “Test methods for Evaluating Material Compatibility in Compressed Hydrogen Applications – Metals”
  - Slow Rising Load Tests



# Fracture Toughness Tests in Hydrogen

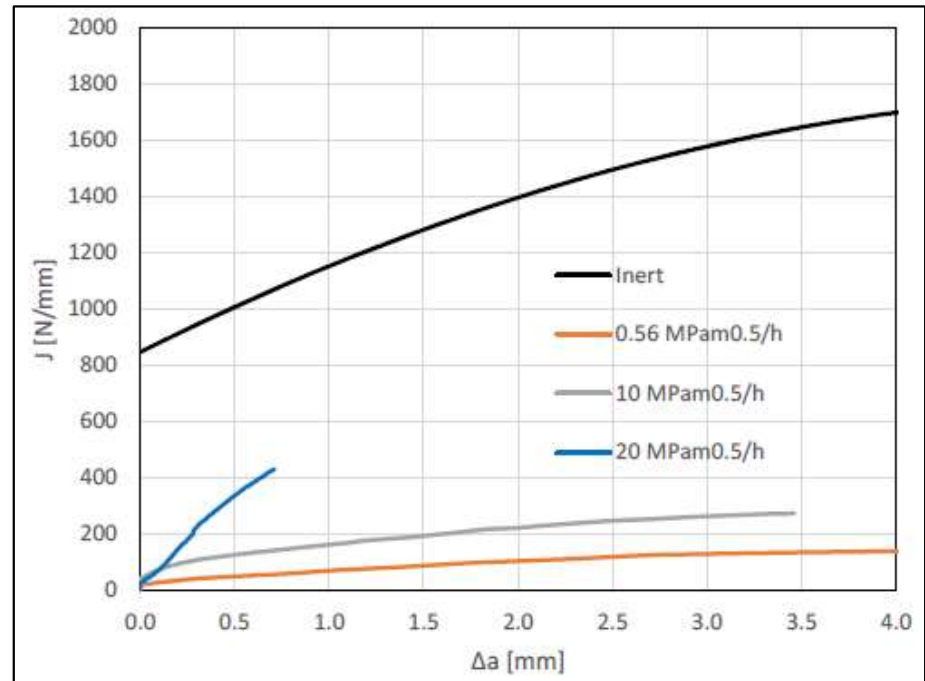
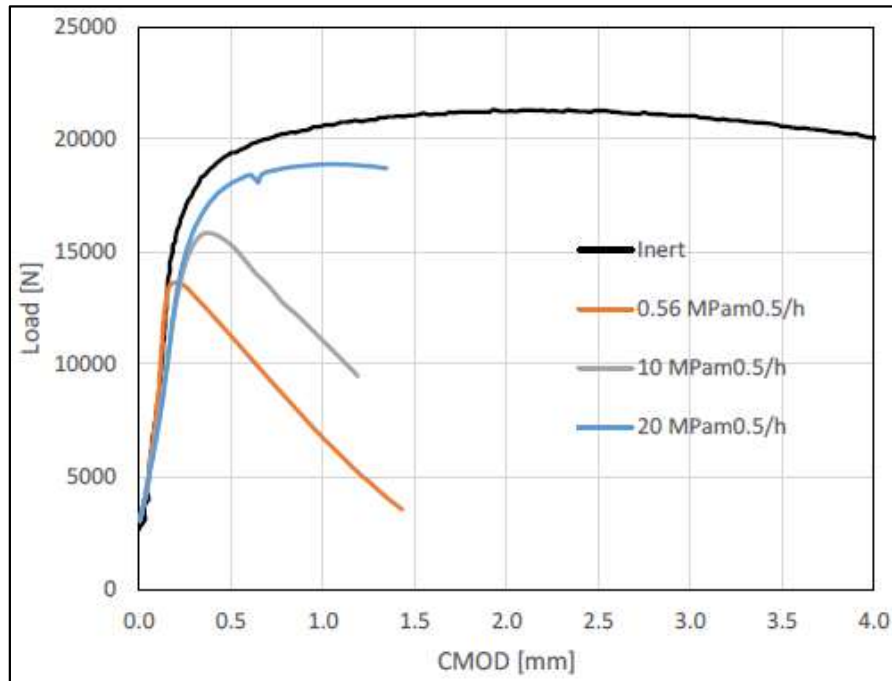
## ASME B31.12 – 2019:

- ASME B31.12 may be well suited for Heavy Wall pressure vessel applications but not hydrogen pipelines (Thinner Wall).
- ASME B31.12 should be limited to ranking materials and demonstrate hydrogen compatibility.

## ANSI / CSA CHMC 1-2014

- ANSI / CSA CHMC 1-2014 is much closer to Best Practice.
  - Slow Rising Load Tests (0.1 – 1.0 MPa√m/minute)
  - Underlying Standard ASTM E1820 (J / CTOD)
  - CT or SENB Specimens
  - Initiation Toughness defined as  $J_{0.2/BL}$  or  $CTOD_{0.2/BL}$

# Hydrogen Embrittlement (DNV JIP)



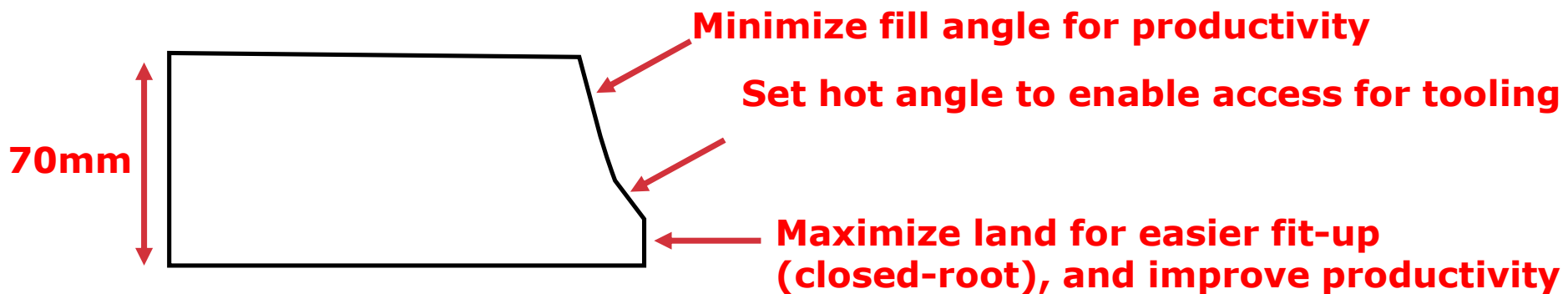
## ANSI / CSA CHMC 1-2014

- The Loading Rates specified in ANSI / CSA CHMC 1-2014 are an order of magnitude faster than typical Loading Rates for Sour Service Tests:
  - 0.1 – 1.0 MPa√m/minute : (ANSI / CSA CHMC 1-2014)
  - 0.01 – 0.1 MPa√m/minute : (Sour Service)
- Reducing the Loading rate will produce a lower J or CTOD R-Curve and may reduce Initiation Toughness.
- There is extensive sour service Test Data to support the Loading Rates used in Sour Service Tests.

## Application: Hydrogen Transport Ship

- Project commissioned by Provaris Energy Ltd. in support of their compressed hydrogen ship program.

- Proprietary multi-layered hydrogen tank comprised of a stainless steel liner layer and 5 structural layers of 70mm thick high-strength steel plate with a SMYS of 80 ksi (550 MPa).
- Fatigue testing is required to prove the resistance of the longitudinal 2G seam weld to high-stress low-cycle fatigue due to pressure cycling during loading and unloading
- CRC Evans : Develop Weld Procedures to Optimize Fatigue Performance.
- CFER Technologies : Fatigue Analysis and Small & Large Scale Fatigue Tests.

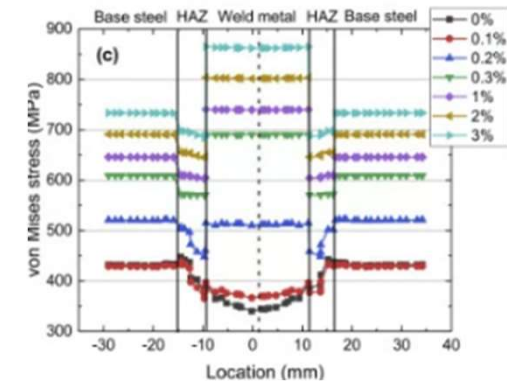
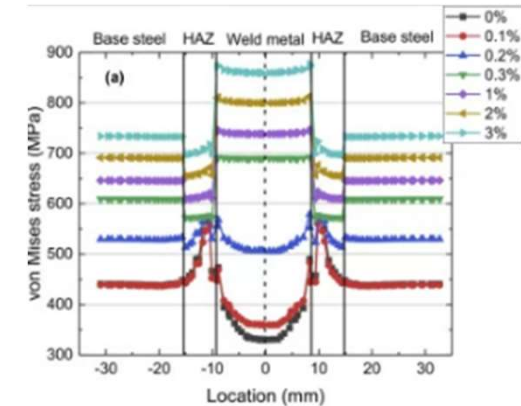




# Criticality of Weld Root

The weld root is critical for several reasons:

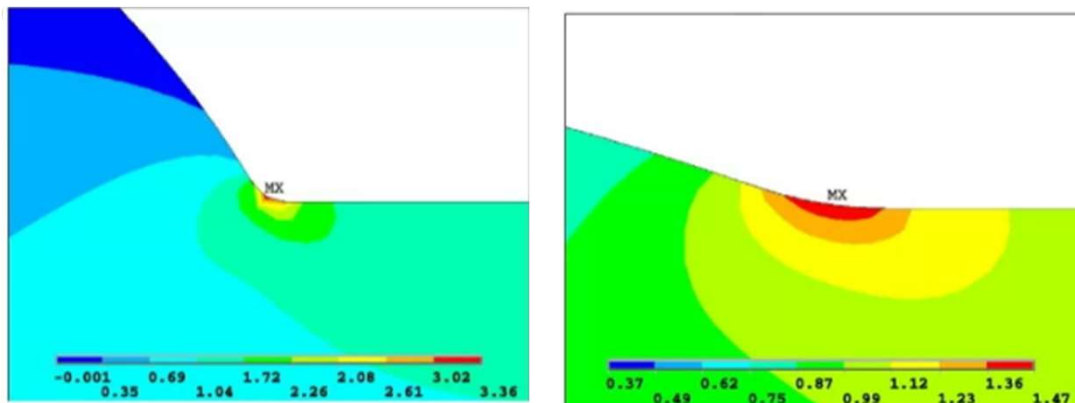
- 1) Geometry of Weld toes serve as stress risers for crack initiations
- 2) Typical single sided weld joints (ex. "V") tend to cause deflection toward the weld cap causing residual tensile stresses in the root
- 3) Root is exposed to the high pressure hydrogen environment directly with highest anticipated concentrations of hydrogen at the weld toes<sup>2</sup>
- 4) Misalignment of pipe joints (Hi/Lo) can result in further elevation of stresses in the joint
- 5) Most sensitive pass where fit-up, and technique are vital to producing a quality bead



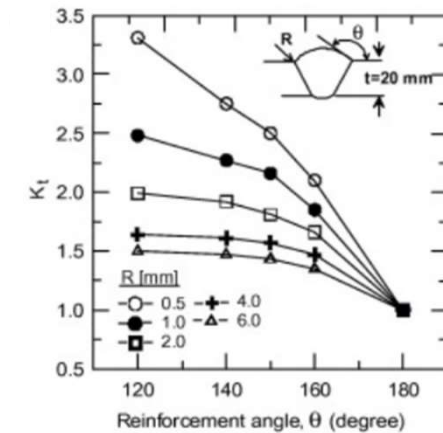
Modelled Von Mises stresses in an X80 girth weld near weld root (top) and cap (bottom)<sup>2</sup>

# Root Geometry

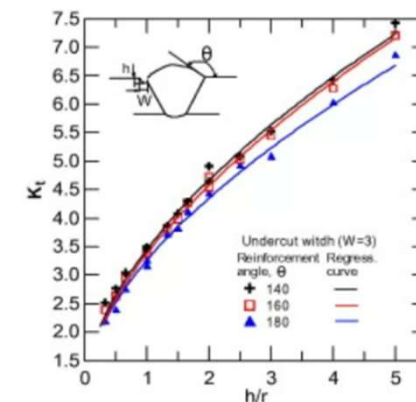
- The magnitude of stress risers at the weld toe are greatly influenced by the radius and contact angle of the reinforcement
- Reinforcement with large contact angles and small radius discourages crack initiation
- Internal undercut can massively increase the stress concentration factor



Map of stress concentration factor in weld reinforcement at large contact angles (left) and small contact angles (right)<sup>3</sup>



Effect of reinforcement radius and contact angle on stress concentration factor<sup>3</sup>

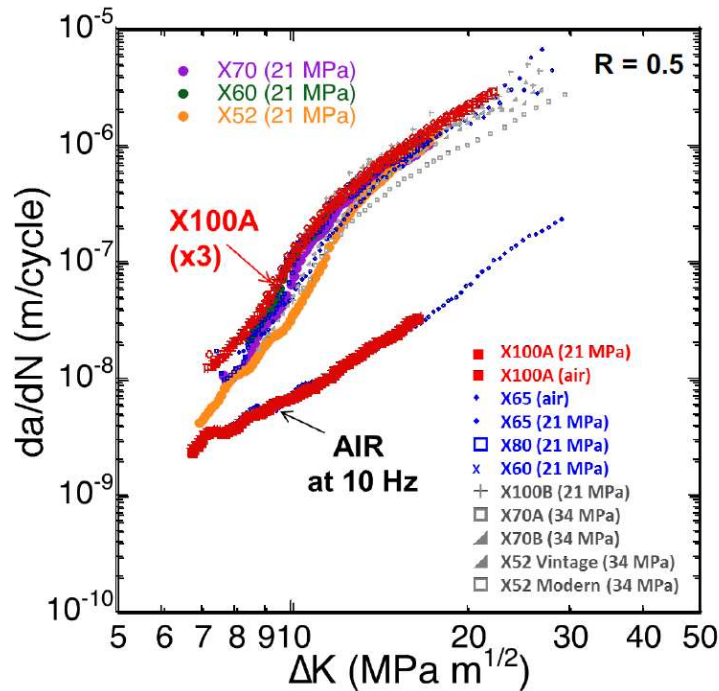


Effect of undercut width on stress concentration factor<sup>3</sup>

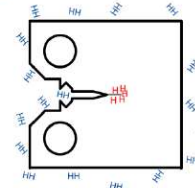
# Hydrogen Gas Transport Modules

- Unlike Hydrogen Pipelines, Gas Transport Modules experience very High Fatigue Demand due to large Pressure Cycles.
- Fatigue and Fracture Performance of Seam Welds is Critical.
- It is important to ensure that the Weld Procedure produces a smooth Defect Free root weld to enhance fatigue performance.
- Need to optimize and verify Root Weld S-N Fatigue Performance.

# Fatigue Crack Growth in Hydrogen



- A wide variety of pipeline steels display nominally the same fatigue response in high-pressure gaseous hydrogen
- The effect of pressure on fatigue crack growth rates is modest for high-pressure hydrogen

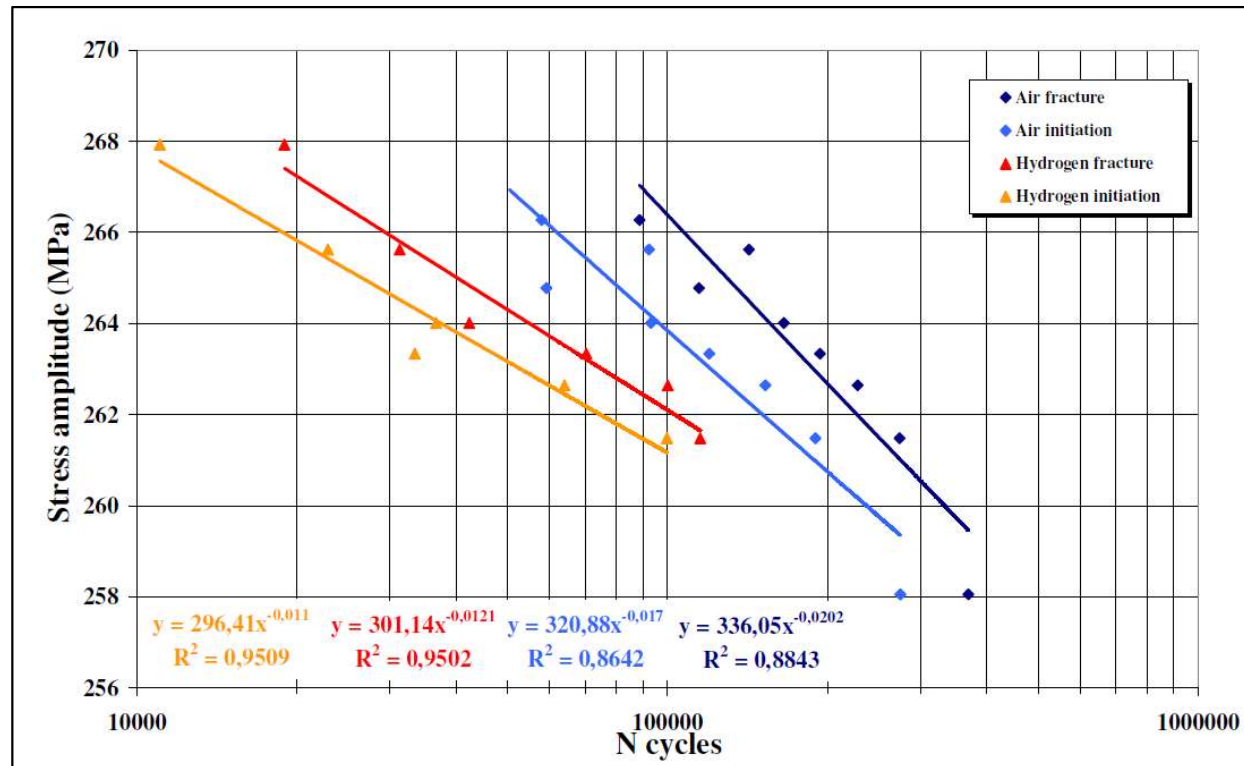


Crack Growth Acceleration Factor (CGAF) can vary from 5 (low  $\Delta K$ ) to 30-50 (high  $\Delta K$ ).

Low partial pressure of hydrogen has nominally same effect as pure hydrogen on pipeline steels

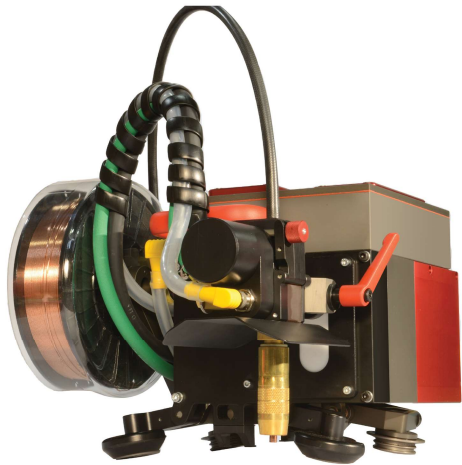
# S-N Fatigue Performance in Hydrogen

- The S-N Knock Down Factor (KDF) is higher at High Stress Ranges (Consistent with FCGR Test Results).



# Design of Root Pass: Overview

- Mechanized root (CRC-Evans M500 Welding Bug) to minimize operator error, and improve quality/consistency
- 3 modified short-arc processes compared (Miller RMD, Fronius CMT, and Fronius LSC)



# Determination of Intensity and Distribution Parameter of Heat Source

- 1G Rotated – Bead on Pipe tests
- Maximized Wire Feed Speed for each process, then tested range of Travel Speeds to fit to thermodynamic model<sup>5</sup>

$$z_{max} \quad \Pi \quad \frac{q}{2\pi k (T_c - T_0)} \quad f(Ry) \cdot g(Ry, \sigma^*)$$

$$f \quad \left[ 1 + \left( \frac{2}{eRy} \right)^{n_1} \right]^{1/n_1}$$

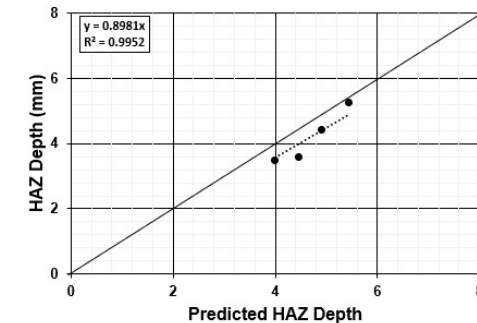
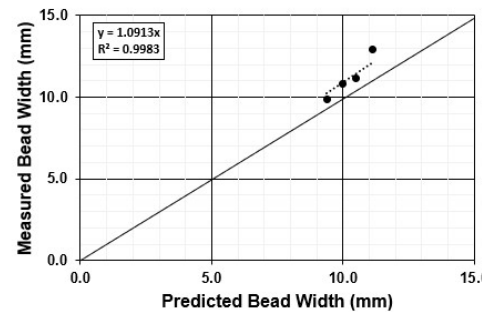
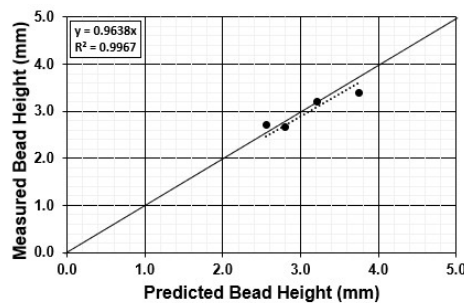
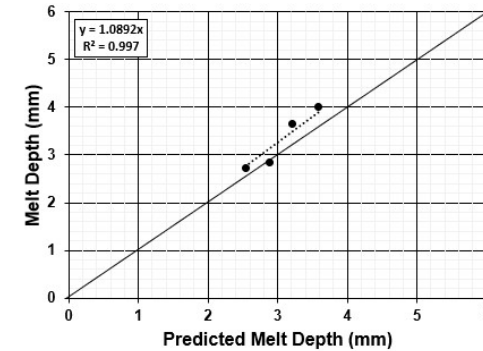
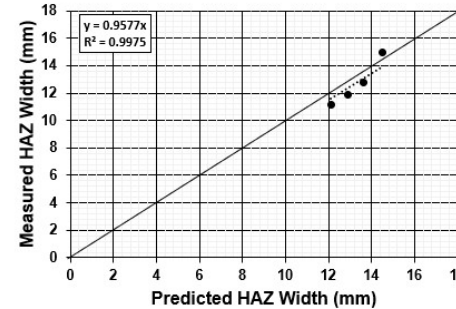
$$g \quad \left\{ 1 + \left\{ \frac{\pi}{2} \ln \left( \frac{\sigma_{max}^*}{\sigma^*} \right) \left[ 1 + \left( 1.495Ry^{-\frac{1}{6}} \right)^{n_3} \right]^{1/n_3} \right\}^{n_2} \right\}^{1/n_2}$$

$$n_1 = -1.47$$

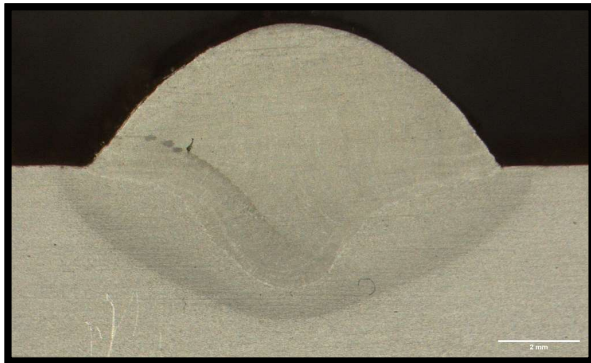
$$n_2 = -1.96 \quad 9.7$$

$$n_3 = -3.22 \quad ***$$

$$**$$

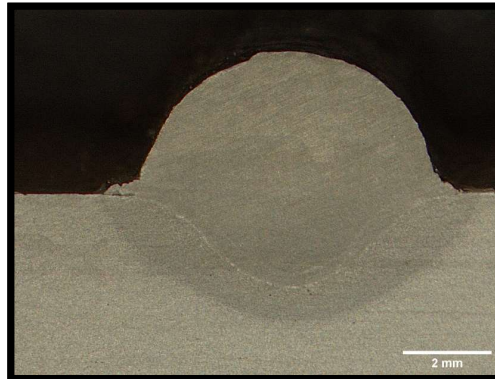


# Comparison of Root Processes (1G Bead on Pipe)



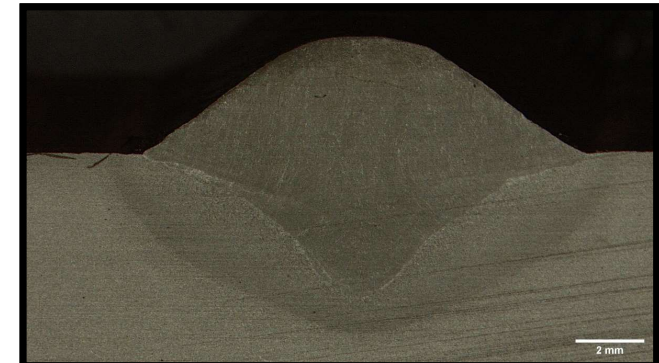
## CMT

Distribution Parameter ( $\sigma$ ): 2.3mm  
Max Intensity: 233W/mm<sup>2</sup>  
Max Instantaneous Power: 4228W  
Travel Speed: 10ipm  
Deposition Rate: 7.7lbs/hr  
Penetration (bead on pipe): 2.9mm



## RMD

Distribution Parameter ( $\sigma$ ): 1.2mm  
Max Intensity: 638W/mm<sup>2</sup>  
Max Instantaneous Power: 2886kW  
Travel Speed: 12ipm  
Deposition Rate: 5.9lbs/hr  
Penetration (bead on pipe): 2.1mm



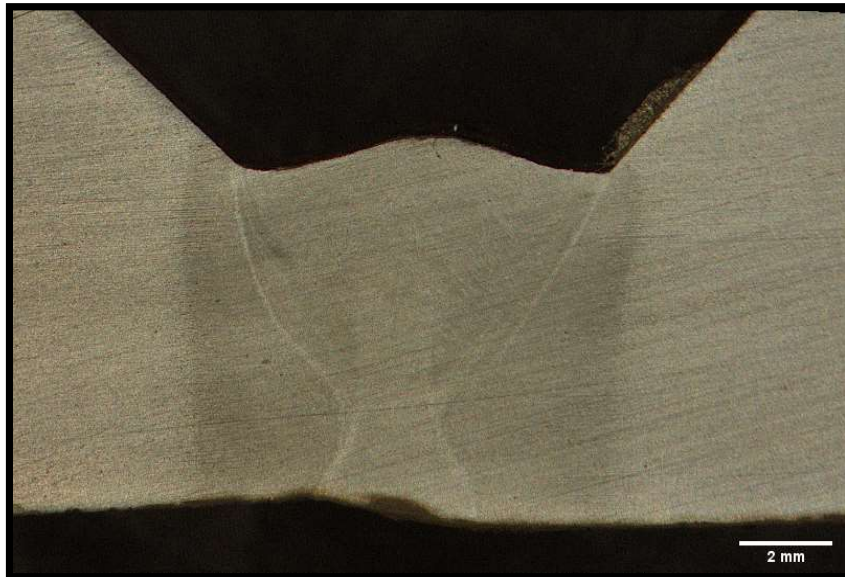
## LSC

Distribution Parameter ( $\sigma$ ): 2.5mm  
Max Intensity: 316W/mm<sup>2</sup>  
Max Instantaneous Power: 6278W  
Travel Speed: 12ipm  
Deposition Rate: 9.3lbs/hr  
Penetration (bead on pipe): 4mm

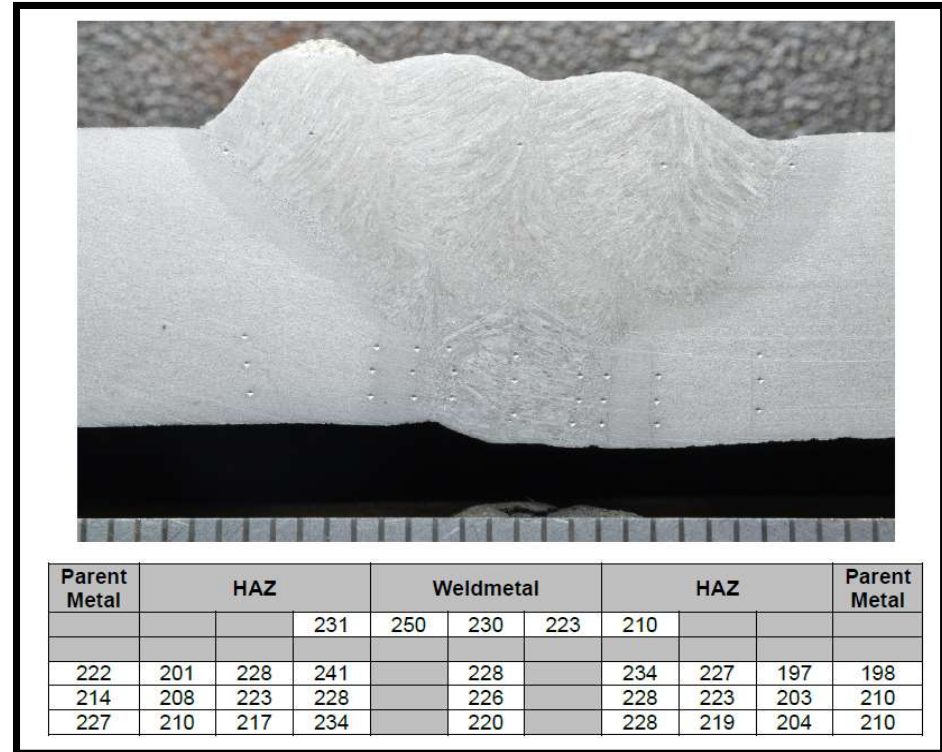
**Larger Intensity produces deeper penetration, whilst larger distribution parameter results in broader, shallower penetration. An ideal process for maximum land has a combination of large intensity and distribution parameter.**



# Root Process in 2G Bevel and Finalized Weld Design



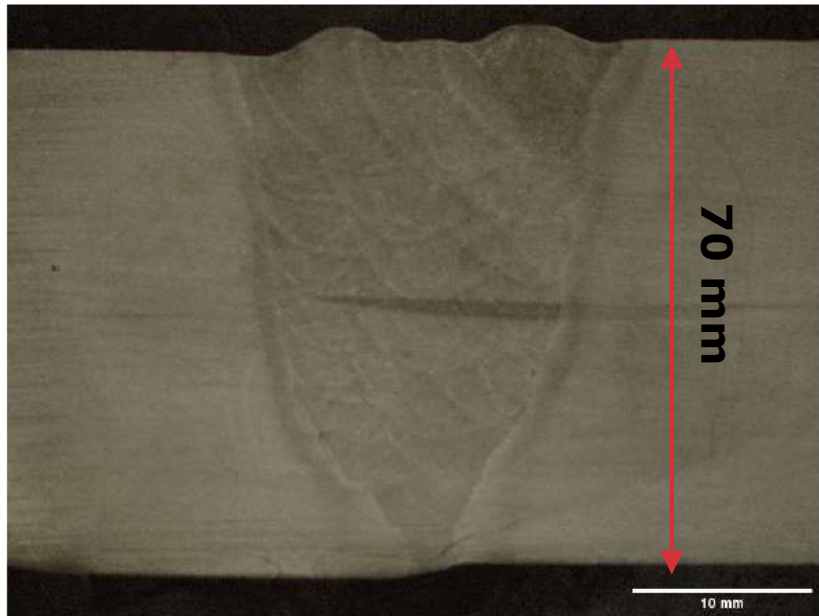
LSC Root in 45° bevel



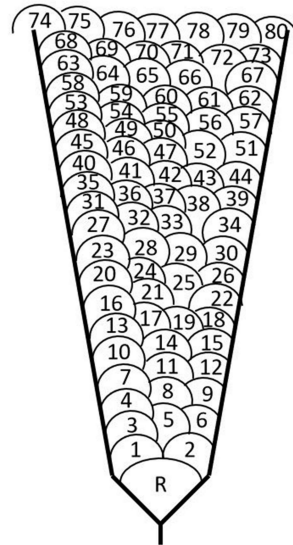
Preliminary weld to evaluate hardness

# Final Large Scale Specimens

(ref. Provaris Energy compressed H<sub>2</sub> ship project)



Cross-Section of Final Weld (taken from run-off tabs)



8' x 4' Fatigue Specimen  
2.76 inches thick

# Final Large Scale Specimens

(ref. Provaris Energy compressed H2 ship project)



As-welded root profile



As-welded cap profile

Pass	Wire Feed Speed (ipm)	Current (A)	Voltage (V)	True Energy (kJ/in)	Travel Speed (ipm)
Top	280	200	19.6	18.6	14.4
GMAW	350	240	20.1	16.7	19.9
Root	315	279	22.5	25.4	14.9

Power Source	Fronius TPS 400i
Pulse Program	Root: LSC Adv. Remaining: PMC
Motion Control	M500 Single Torch Bug
Shielding Gas	90%Ar / 10% CO <sub>2</sub>
Wire	ER100S-1

# Summary

- CRC / Microalloying are actively engaged in Weld Procedure Development and Qualification for:
  - Hydrogen Pipelines
    - API 1104 Hydrogen Task Group
    - ECA / Girth Weld Toughness Test Procedures
  - Hydrogen Gas Transport Modules.
    - Weld Root Optimization
    - Full-Scale S-N Fatigue Testing



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